

# Mathematical Modeling of Upflow Anaerobic Sludge Blanket Reactor in Domestic Wastewater Treatment

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**Abstract:** This paper introduces a dynamic model to describe the behavior of an upflow anaerobic sludge blanket (UASB) reactor. The model is based on the mass and energy balances of the reactor. The model is used to study the effect of various operating parameters on the reactor performance. The results show that the reactor performance is highly sensitive to the inlet substrate concentration and the hydraulic retention time.

**Indexing:** UASB reactor, dynamic model, wastewater treatment.

$$S = S_0 - \frac{1}{Y} \left( \frac{dX}{dt} + \frac{dV}{dt} X \right)$$

**A** mathematical model is developed to describe the behavior of an upflow anaerobic sludge blanket (UASB) reactor. The model is based on the mass and energy balances of the reactor. The model is used to study the effect of various operating parameters on the reactor performance. The results show that the reactor performance is highly sensitive to the inlet substrate concentration and the hydraulic retention time.

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$$\frac{dS}{dt} = \frac{1}{V} (Q_0 S_0 - Q_1 S) + R_S Y$$

$$\phi = \sqrt{\frac{1}{Y} \left( \frac{dX}{dt} + \frac{dV}{dt} X \right)}$$

The model is used to study the effect of various operating parameters on the reactor performance. The results show that the reactor performance is highly sensitive to the inlet substrate concentration and the hydraulic retention time.

$f_{CO_2} = 0.10$   
 $f_{CH_4} = 0.15$   
 $f_{H_2O} = 0.20$

Substrate concentration degradation at (a) various dispersion coefficients, and (b) different fractions of reactor volume occupied by granules

Fig.1. Substrate concentration degradation at (a) various dispersion coefficients, and (b) different fractions of reactor volume occupied by granules

$$V_1 \frac{dC_{S1}}{dt} = F_o C_{S1} - F_{12} C_{S1} - R_{S1} V_1$$

$$V_2 \frac{dC_{S2}}{dt} = F_{12} C_{S1} + SF F_m C_{S1} - F_{21} C_{S2} - F_m C_{S2} - R_{S2} V_2$$

$$R_S = (\mu - K_d) \frac{C_X}{Y}, \quad \frac{dC_{S3}}{dt} = D \frac{\partial^2 C_{S3}}{\partial z^2} - W \frac{\partial C_{S3}}{\partial z}$$

$$F_m = SF F_m + F_o, \quad F_{12} = F_{21} + F_o$$

$$D_{80} \sim \dots \sim X \cdot F_{21} = q_{gb} \left( \frac{10}{10 + h_2 + h_3} \right)$$

**B. Model proposed by Parsamehr, Sweden**

$$R_{CH_4} = f_{CH_4} \frac{(1-Y) \mu_1 C_{X1}}{Y}$$

$$f = \frac{f_{max} C_{CH_4}}{K_{CH_4} + C_{CH_4}}$$

$$C_{HS} = \frac{10^{-pH} C_S}{K_A + 10^{-pH}} \quad (13)$$

Substrate concentration degradation at (a) in reactor bed zone versus time, and (b) in reactor blanket zone versus time, and gases concentration produced (c) in reactor bed zone versus time, and (d) in reactor blanket zone versus time

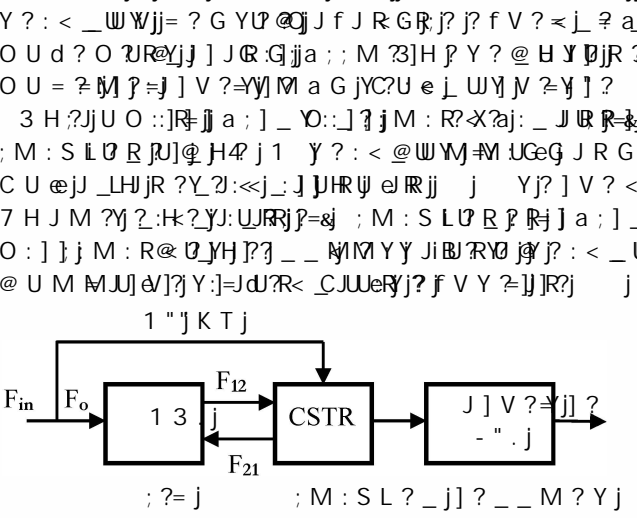


Fig.2. A schematic block diagram for hydraulic model of the UASB reactor

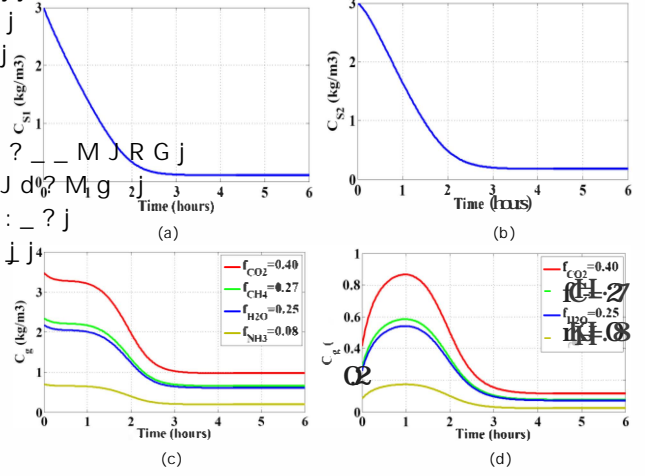


Fig.3. Substrate concentration degradation (a) in reactor bed zone versus time, and (b) in reactor blanket zone versus time, and gases concentration produced (c) in reactor bed zone versus time, and (d) in reactor blanket zone versus time

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Time (hrs) (a) Time (hrs) (b)

Fig.4. (a) Substrate concentration degradation in the UASB reactor versus time, and (b) The effective biomass concentration in the UASB reactor versus time

$$C_{Si} = C_{Si0} \exp(-\mu_{max} t)$$

$$X_{eff} = X_{max} \left( \frac{C_{Si}}{C_{Si0}} \right)^n$$

A. Previous experimental results

The effect of bacterial growth rate on reactor bed zone performance is shown in Fig. 5(a). The substrate concentration  $C_{Si}$  (kg/m<sup>3</sup>) decreases over time (0 to 6 hours) for three different maximum growth rates:  $\mu_{max} = 0.040$  day<sup>-1</sup> (green line),  $\mu_{max} = 0.035$  day<sup>-1</sup> (blue line), and  $\mu_{max} = 0.030$  day<sup>-1</sup> (red line). Higher growth rates result in faster substrate degradation.

$$E_{COD} = \frac{C_{Si0} - C_{Si}}{C_{Si0}}$$

$$E_{COD} = \frac{C_{Si0} - C_{Si}}{C_{Si0}} + \left( \frac{C_{Si}}{C_{Si0}} \right)^s$$

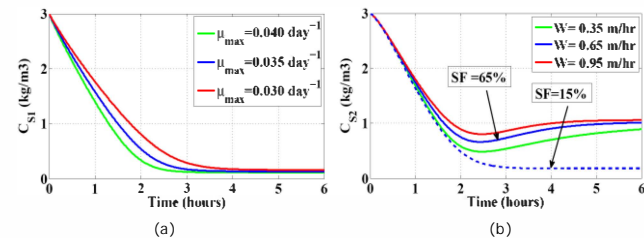


Fig.5. (a) Effect of bacterial growth rate on reactor bed zone performance, and (b) Effect of upflow velocity and bypass flow fraction on reactor blanket zone performance

B. Developed model for VASE reactor

The developed model for the VASE reactor is based on the following assumptions:

- 1. The reactor is divided into a bed zone and a blanket zone.
- 2. The substrate concentration in the bed zone is  $C_{Si}$  and in the blanket zone is  $C_{Sb}$ .
- 3. The biomass concentration in the bed zone is  $X_{b1}$  and in the blanket zone is  $X_{b2}$ .
- 4. The upflow velocity is  $W$  and the bypass flow fraction is  $SF$ .

The substrate balance in the bed zone is given by:

$$Q_{in} C_{Si0} - Q_{out} C_{Si} - V_{bed} \mu_{max} C_{Si} X_{b1} = 0$$

The substrate balance in the blanket zone is given by:

$$Q_{in} C_{Si} - Q_{out} C_{Sb} - V_{blanket} \mu_{max} C_{Sb} X_{b2} = 0$$

The biomass balance in the bed zone is given by:

$$Q_{in} X_{b1} - Q_{out} X_{b1} - V_{bed} \mu_{max} C_{Si} X_{b1} = 0$$

The biomass balance in the blanket zone is given by:

$$Q_{in} X_{b2} - Q_{out} X_{b2} - V_{blanket} \mu_{max} C_{Sb} X_{b2} = 0$$

C. Sensitivity analysis for developed model

The sensitivity analysis for the developed model is performed by varying the parameters  $\mu_{max}$ ,  $W$ , and  $SF$ . The results show that the substrate concentration degradation is most sensitive to changes in  $\mu_{max}$ .

Figure 6 shows the substrate concentration degradation in the reactor bed zone (a) and in the reactor blanket zone (b) versus time. The Parsamehr model is compared with the Developed model. The substrate concentration  $C_{Si}$  (kg/m<sup>3</sup>) decreases over time (0 to 6 hours). The developed model shows a better fit to the experimental data than the Parsamehr model.

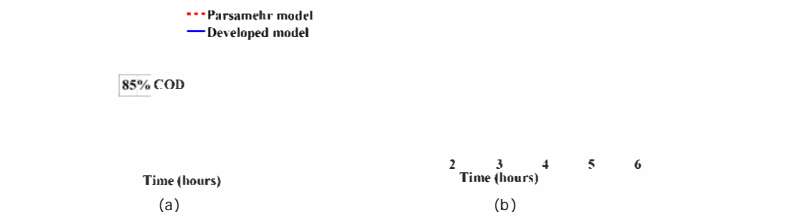


Fig.6. Substrate concentration degradation (a) in reactor bed zone versus time, and (b) in reactor blanket zone versus time

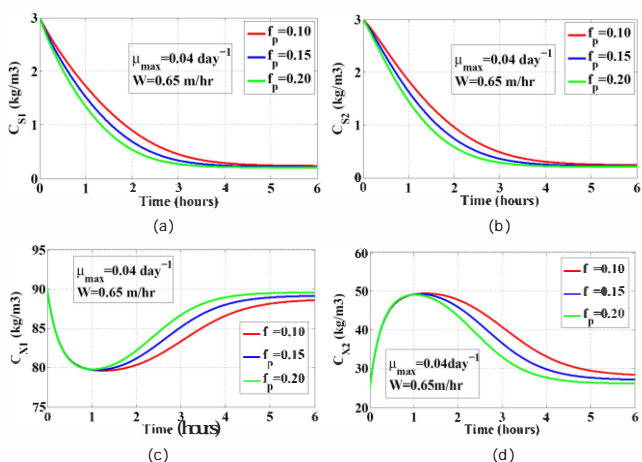


Fig.7. Substrate concentration in the UASB reactor (a) bed zone versus time and (b) blanket zone versus time, and Biomass concentration in the UASB reactor (c) bed zone versus time and (d) blanket zone versus time

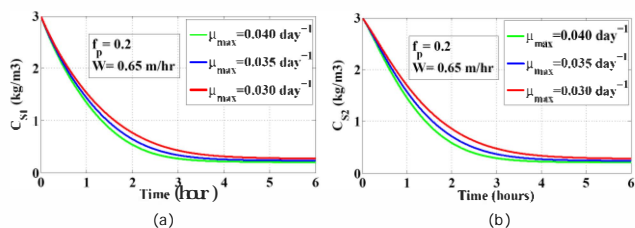


Fig.8. Substrate concentration in the UASB reactor (a) bed zone versus time, and (b) blanket zone versus time

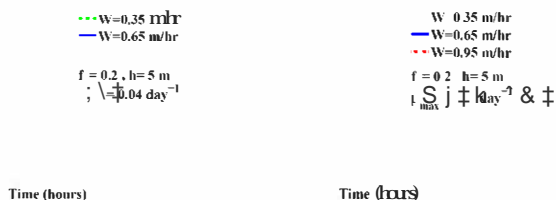


Fig.9. Substrate concentration in the UASB reactor (a) bed zone versus time, and (b) blanket zone versus time

$J, \phi$	fraction of volume fraction occupied by granules	—
$V_H$	height of reactor	m
$K, k$	chemical reaction constant	$hr^{-1}$
$k_L$	mass transfer coefficient	m/hr
$K_A, K_1, K_s$	substrate inhibition constants	$kg/m^3$
$K_d$	decay constant	$hr^{-1}$
$U$	upflow velocity	$m/hr$
$> \phi$	organic degradation BOD	$kg/m^3 \cdot day$
$r_{dr}$	dragging efficiency	%
$A$	radius of biological granule	m
$R_{CH}, R_s$	methanogenesis rate	$kg/m^3 \cdot hr$
$S$	sludge thickness	cm
$e, \tau$	various hydraulic retention time	hours
$G$	volume of reactor	$m^3$
$H_c, J$	settling and upflow velocities	$m/hr$
$X$	drag coefficient of biomass	$m^3/m^3$
$h$	yield coefficient of biomass per substrate	$kg/kg$
$Z$	vertical height of reactor	m

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ABBREVIATIONS

Symbol	Definition	Unit
$5 \phi$	cross-sectional area of reactor	$m^2$
$CHSS, C_{SO}, C_{SM}$	unionized, volatile and non-volatile substrate concentration	$kg/m^3$
$C_X, C_{X0}$	various time and initial biomass concentration	$kg/m^3$
$D, D_A$	dispersion and effective diffusion coefficients	$m^2/hr$
$E$	substrate conversion efficiency	%
$F_{in}$	influent wastewater discharge	$m^3/hr$